

ML145145 4–Bit Data Bus Input PLL Frequency Synthesizer

INTERFACES WITH SINGLE–MODULUS PRESCALERS

Legacy Device: *Motorola MC145145-2*

The ML145145 is programmed by a 4–bit input, with strobe and address lines. The device features consist of a reference oscillator, 12–bit programmable reference divider, digital phase detector, 14–bit programmable divide–by–N counter, and the necessary latch circuitry for accepting the 4–bit input data.

- Operating Temperature Range: $T_A 40$ to 85 \degree C
- Low Power Consumption Through the Use of CMOS Technology
- 3.0 to 9.0 V Supply Range
- Single Modulus 4–Bit Data Bus Programming
- \div N Range = 3 to 16,383, \div R Range = 3 to 4,095
- "Linearized" Digital Phase Detector Enhances Transfer Function Linearity
- Two Error Signal Options: Single–Ended (Three–State) Double–Ended

becomes available, will be identified by a part number prefix change from **ML** to **MLE**.

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MAXIMUM RATINGS* (Voltages Referenced to VSS)

This device contains protection circuitry to guard against damage due to high static voltages or electric fields. However, precautions must be taken to avoid applications of any voltage higher than maximum rated voltages to these high-impedance circuits. For proper operation, Vin and Vout should be constrained to the range $V_{SS} \leq (V_{in} \text{ or } V_{out}) \leq V_{DD}$.

Unused inputs must always be tied to an encode when we can appropriate logic voltage level (e.g., either V_{SS} or V_{DD}), except for inputs with pull-up devices.
Unused outputs must be left open.

*Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables or Pin Descriptions section.

†Power Dissipation Temperature Derating:

Plastic DIP: -12 mW/°C from 65 to 85°C

SOG Package: - 7.0 mW/°C from 65 to 85°C

ELECTRICAL CHARACTERISTICS (Voltages Referenced to V_{SS})

(continued)

ELECTRICAL CHARACTERISTICS (continued)

AC ELECTRICAL CHARACTERISTICS (C_L = 50 pF, input t_f = t_f = 10 ns)

* Includes all probe and fixture capacitance.

Figure 5. Test Circuit

V_H = High voltage level.
V_L = Low voltage level.
* At this point, when both f_R and f_V are in phase, the output is forced to near mid supply.
* At this point, when both f_R and f_V are in phase, the output is forc output is high impedance and the voltage at that pin is determined by the low-pass filter capacitor.

Figure 6. Phase/Frequency Detectors and Lock Detector Output Waveforms

PIN DESCRIPTIONS

INPUT PINS

D0 – D3

Data Inputs (PDIP – Pins 2, 1, 18, 17; SOG – Pins 2, 1, 20, 19)

Information at these inputs is transferred to the internal latches when the ST input is in the high state. D3 is most signigicant bit.

fin

Frequency Input (PDIP – Pin 3, SOG – Pin 4)

Input to $\div N$ portion of synthesizer. f_{in} is typically derived from the loop VCO and is ac couples. For larger amplitude signals (standard CMOS – logic levels) dc coupling may be used.

OSCin/OSCout

Reference Oscillator Input/Output (PDIP – Pins 6, 7; SOG – Pins 7, 8)

These pins form an on–chip reference oscillator when connected to terminals of an external parallel resonant crystal. Frequency setting capacitors of appropriate value must be connected from OSC_{in} to ground and OSC_{out} to ground. OSC_{in} may also serve as input for an externally–generated reference signal. This signal is typically AC coupled to \rm{OSC}_{in} but for larger amplitude signals (standard CMOS–logic levels) DC coupling may also be used. In the external refrence mode, no connection is required to $\rm OSC_{out}$.

A0 – A2

Address Inputs (PDIP – Pins 8, 9, 10; SOG – Pins 9, 10, 12)

A0, A1 and A2 are used to define which latch receives the information on the data input lines. The addresses refer to the following latches:

ST

Strobe Transfer (PDIP – Pin 11, SOG – Pin 13)

The rising edge of strobe transfers data into the addressed

latch, the falling edge of strobe latches data into the latch. This pin should normally be held low to avoid loading latches with invalid data.

OUTPUT PINS

PDout

Single–Ended Phase Detector output (PDIP – Pin 12, SOG – Pin 14)

Three–state output of phase detector for use as loop–error signal.

Frequency $f_V > f_R$ or f_V Leading: Negative Pulses

Frequency $f_V < f_R$ or f_V Lagging: Positive Pulses

Frequency $f_V = f_R$ and Phase Coincidence: High–Impedance State

LD

Lock Detector Signal (PDIP – Pin 13, SOG – Pin 15)

High level when loop is locked (fR, fV) of same phase and frequency). Pulses low when loop is out of lock. φ**V,** φ**R**

Phase Detect or Outputs (PDIP – Pin 12, SOG – Pin 14)

These phase detector outputs can be combined externally for a loop–error signal. A single–ended output is also available for this purpose (see PD_{out}).

If frequency fy is greater than f_R or if the phase of fy is leading, then error information is provided by φV pulsing low. φR remains essentially high.

If the frequency of $fy - fR$ and both are in phase, then both φV and φR remain high except for a small minimum time period when both pulse low in phase.

REFout

Buffered Reference Output (DIP – Pin 16, SOG – Pin 18)

Buffered output of on–chip reference oscillator or externally provided reference–input signal.

POWER SUPPLY PINS

VSS

Ground (PDIP – Pin 4, SOG – Pin 5)

Circuit Ground

VDD

Positive Power Supply (PDIP – Pin 5, SOG – Pin 6)

The positive supply voltage may range from 3.0 to 9.0 V with respect to VSS.

DESIGN CONSIDERATIONS

PHASE-LOCKED LOOP - LOW-PASS FILTER DESIGN

NOTE: Sometimes R₁ is split into two series resistors, each R₁ + 2. A capacitor C_C is then placed from the midpoint to ground to further filter ϕ_V and ϕ_R . The value of C_C should be such that the corner frequency of this network does not significantly affect ω_R .

(at phase detector input).

DEFINITIONS:

N = Total Division Ratio in feedback loop K_{φ} (Phase Detector Gain) = $V_{DD}/4\pi$ for PD_{OUI}
 K_{φ} (Phase Detector Gain) = $V_{DD}/2\pi$ for ϕ_V and ϕ_R

 K_{VCO} (VCO Gain) = $\frac{2\pi\Delta f_{VCO}}{\Delta V_{VCO}}$

for a typical design w_n (Natural Frequency) $\approx \frac{2\pi \text{fr}}{10}$

Damping Factor: $\zeta \equiv 1$

CRYSTAL OSCILLATOR CONSIDERATIONS

The following options may be considered to provide a reference frequency to Motorola's CMOS frequency sytnthesizers.

Use of a Hybrid Crystal Oscillator

Commercially available temperature–compensated crystal oscillators (TCXOs) or crystal–controlled data clock oscillators provide very stable reference frequencies. An oscillator capable of sinking and sourcing 50 µA at CMOS logic levels may be direct or DC coupled to OSC_{In}. In general, the highest frequency capability is obtained utilizing a direct–coupled square wave having a rail–to–rail $(VDD$ to $VSS)$ voltage swing. If the oscillator does not have CMOS logic levels on the outputs, capacitive or AC coupling to OSCin may be used. $\mathrm{OSC}_{\mathrm{out}}$, and unbuffered output, should be left floating.

For additional information about TCXOs and data clock oscillators, please consult the latest version of the *eem Electronic Engineers Master Catalog*, the *Gold Book*, or similar publications.

Design an Off–Chip Reference

The user may design an off–chip crystal oscillator using ICs specifically developed for crystal oscillator applications, such as the ML12061 MECL device. The reference signal from the MECL device is ac coupled to \rm{OSC}_{in} . For large amplitude sig-OSCout, an unbuffered output, should be left floating. In general, the highest freqency capability is obtained with a direct–coupled square wave having rail–to–rail voltage swing. nals (standard CMOS logic levels), DC coupling is used.

Use of the On–Chip Oscillator Circuitry

The on–chip amplifier (a digital inverter) along with an appropriate crystal may be used to provide a reference source frequency. A fundamental mode crystal, parallel resonant at the desired operating frequency, should be connected as shown in Figure 7.

For V_{DD} = 5.0 V, the crystal should be specified for a loading capactitanc. CL, which does not exceed 32 pf for frequencies to approximately 8.0 to 15 MHz and 10 pF for higher frequencies. These are guidelines that provide a reasonable compromise between IC capacitance, drive capability, swamping c–variations in stray and IC input/output capacitance, and realistic C_{L} values. The shunt load capacitance. C_{L} , presented across the crystal can be estimated to be:

$$
C_L = \frac{C_{in}C_{out}}{C_{in} + C_{out}} + C_a + C_0 + \frac{C1 \cdot C2}{C1 + C2}
$$

where

 $Cin = 5.0$ pf (see Figure 8) Cout = 6.0 pf (see Figure 8) $Ca = 1.0$ pf (see Figure 8) $CO =$ the crystal's holder capacitance (see Figure 9) C1 and $C2$ = external capacitors (see Figure 7)

The oscillator can be "trimmed" on–frequency by making a

portion of all of C1 variable. The crystal and associated components must be located as close as possible to the OSC_{in} and OSCout pins to minimize distortion, stray capacitance, stray inductance and startup stablilization time. In some cases, stray capacitance should be added to the value for C_{in} and C_{out} .

Power is dissipated in the effective series resistance of the crystal Re, in Figure 9. The drive level specified by the crystal manufacturer is the maximum stress that a crystal can withstand without damage or excessive shift in frequency. R1 in Figure 7 limits the drive level. The use of R1 may not be necessary in some cases (i.e., $R1 = 0 \Omega$)

To verify that the maximum dc supply voltage does not overdrive the crystal, monitor the output frequency as a function of voltage at $\rm OSC_{out}$. (Care should be taken to minimize loading.) The frequency should increase very slightly as the dc supply voltage is increased. An overdriven crystal will decrease in frequency or become unstable with an increase in supply voltage. The operating supply voltage must be reduced or R1 must be increased in value if the overdriven condition exists. The user should note that the oscillator start–up time is proportional to the value of R1.

Through the process of supplying crystals for use with CMOS inverters, many crystal manufactureres have developed expertise in CMOS oscillator design with crystals. Discussions with such manufacturers can prove very helpful (see Table 1).

* May be deleted in certain cases. See text.

Figure 7. Pierce Crystal Oscillator Circuit

Figure 8. Parasitic Capacitances of the Amplifier

NOTE: Values are supplied by crystal manufacturer (parallel resonant crystal).

Figure 9. Equivalent Crystal Networks

NOTE: Lansdale cannot recommend one supplier over another and in no way suggests that this is a complete listing of crystal manufacturers.

Figure 10. TV/CATV Tuning System

RECOMMENDED READING

Technical Note TN–24, Stated Corp.

Technical Note TN–\7, Stated Corp.

E. Hafner, "The Piezoelectric Crystal Unit – Definitions and Method of Measurement", *Proc IEEE*, Vol. 57, No. 2 Feb., 1969

D. Kemper, L. Rosine, "Quartz Crystals for Frequency Control", *Electro–Technology*, June, 1969.

P.J. Ottowitz, "A Guide to Crystal Selection", *Electronic Design*, May, 1966.

LEGACY APPLICATIONS

The features of the ML145145 permit bus operation with a dedicated wire needed only for the strobe input. In a microprocessor–controlled system this strobe input is accessed when the PLL is addressed. The remaining data and address inputs will directly interface to the microprocessor's data and address buses.

The \div R programability is used to advantage in Figure 10. Here, the nominal \div R value is 3667, but by programming small changes in this value, fine tuning is accomplised. Better tuning resolution is achievable with this method than by changing the \div N due to the use of the large fixed prescaling value of \div 256 provided by the ML12079.

The two–loop synthesizer, in Figure 11, takes advantage of these features to control the phase–locked loop with a minumum of dedicated lines while preserving optimal loop performance. Both 25 Hz and 100 Hz steps are provided while the relatively large reference frequencies of 10 Khz or 10.1 kHz are maintained.

NOTES:

1. Table 2 provides program sequence for the + N1 (Loop 1) and + N2 (Loop 2) Counters.

2. $+ R1 = 1000$, fp₁ = 10.1 kHz, $+ R2 = 1010$, fp₂ = 10 kHz.
3. fy_{CO1} = N1(f_{R1}) + N2(fp₂) = N1(f_{R2} + Af) + N2(f_{R2}) where $\Delta f = 100$ Hz.
4. Other f_{R1} and fp₂ values may be used with appropriate $+ N1$ and $+$

Figure 11. Two-Loop Synthesizer Provides 25 and 100 Hz Frequency Steps While Maintaining High Detector Comparison Frequencies of 10 and 10.1 kHz

Table 2. Programming Sequence for Two-Loop Synthesizer of Figure 11

OUTLINE DIMENSIONS

P DIP 18 = VP (ML145145VP) CASE 707–02

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